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Single Crystal Gradient Plasticity – Part III

Chair for Continuum Mechanics – Institute of Engineering Mechanics



Motivation

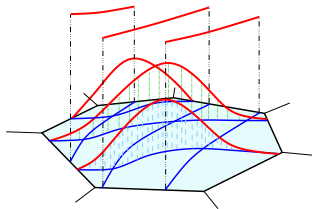
Dislocation continuum theories – overview

The concept of lifted curves

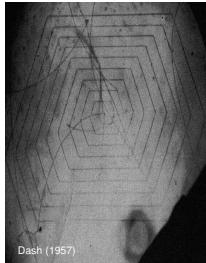
Modelling of pile-ups

Numerical results

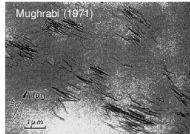
Conclusion and Outlook



- **Fundamental dislocation theory**
e.g. Taylor (1934); Orowan (1935); Schmid and Boas (1935); Hall (1951); Petch (1953)
- **Kinematics and crystallographic aspects of GNDs**
Nye (1953); Bilby, Bullough and Smith (1955); Kröner (1958); Mura (1963); Arsenlis and Parks (1999)
- **Thermodynamic gradient theories**
e.g. Fleck et al. (1994); Steinmann (1996); Menzel and Steinmann (2001); Liebe and Steinmann (2001); Reese and Svendsen (2003); Berdichevski (2006); Ekh et al. (2007); Gurtin, Anand and Lele (2007); Fleck and Willis (2009); Bargmann et al. (2010); Miehe (2011)
- **Slip resistance dependent on GNDs and SSDs**
e.g. Becker and Miehe (2004); Evers, Brekelmans and Geers (2004); Cheong, Busso and Arsenlis (2005)
- **Micromorphic approach**
e.g. Forest (2009); Cordero et al. (2010); Aslan et al. (2011)
- **Continuum Dislocation Dynamics**
e.g. Hochrainer (2006); Hochrainer, Zaiser and Gumbsch (2007); Hochrainer, Zaiser and Gumbsch (2010); Sandfeld, Hochrainer and Zaiser (2010); Sandfeld (2010)



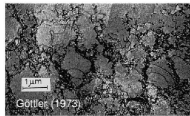
Spiral source



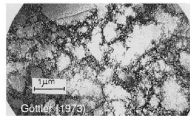
(a)



(b)

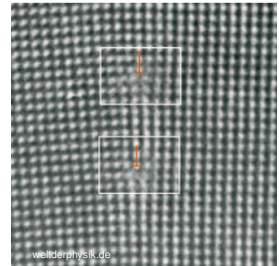


(c)



(d)

Cell structures at different
deformation stages



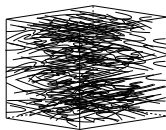
Single dislocations

Important features of the microstructure

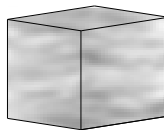
- Total line length/density
- Dislocation motion/transport
- Dislocation sources
- Lattice distortion

Classical Continuum Dislocation Measures

Total line length per unit volume

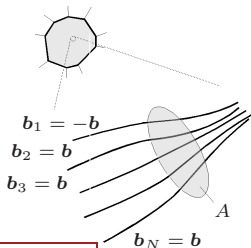


$$\rho = \frac{\Delta l_{\text{tot}}}{\Delta V}$$



Typical (local) evolution law: $\partial_t \rho = f(\dot{\gamma}, \rho)$

Transport neglected!



$$b_{\text{eff}} = \sum_i b_i$$

Nye's dislocation density tensor

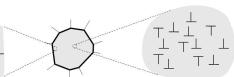
$$\alpha = \text{curl} (H^p)$$

SSDs neglected!

H^p : plastic displ. gradient



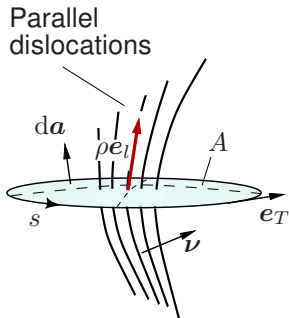
GNDs ✓



SSDs ✗

Smooth Dislocation Bundles

Mura (1963)



Dislocation density vector

$$\boldsymbol{\kappa} := \rho \mathbf{e}_l$$

Effective 'Number' of penetration points

$$N_{\text{eff}} = \int_A \boldsymbol{\kappa} \cdot d\mathbf{a},$$

Dislocation flux into A

$$\dot{N}_{\text{eff}} = - \int_{\partial A} (\boldsymbol{\kappa} \times \boldsymbol{\nu}) \cdot \mathbf{e}_T ds,$$

$$\Rightarrow \partial_t \boldsymbol{\kappa} = -\text{curl}(\boldsymbol{\kappa} \times \boldsymbol{\nu})$$

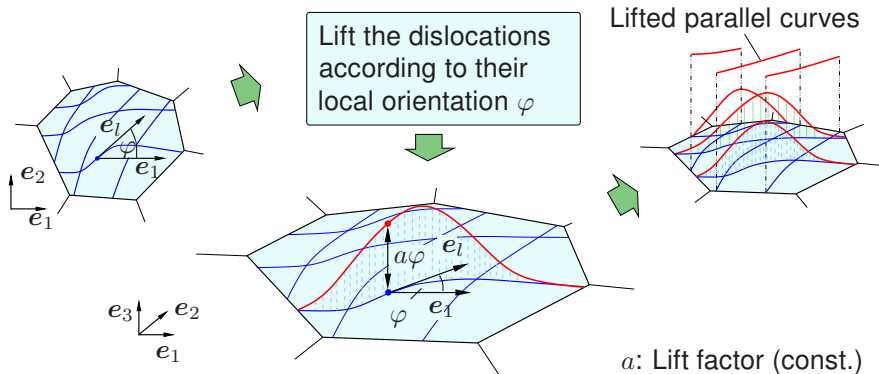
Closed evolution equation

Holds if nearby dislocations are parallel!

How to treat **non-parallel** dislocations?

Concept of lifted dislocations

Hochrainer (2006); Hochrainer, Zaiser and Gumbsch (2007)



If curvature depends on position and orientation $k = k(x_1, x_2, \varphi, t)$:

Adjacent lifted dislocations are **parallel!**

Concept of lifted dislocations

Hochrainer (2006); Hochrainer, Zaiser and Gumbsch (2007)

Density vector of lifted dislocations

$$\kappa^{II} = \rho^{II} e_l^{II}$$

ρ^{II} : Density of lifted dislocations

e_l^{II} : line direction

Velocity of the lifted dislocations

$$\mathbf{V} = \boldsymbol{\nu} + a\vartheta \mathbf{e}_3$$

$\boldsymbol{\nu}$: real dislocation velocity

ϑ : angular velocity

Evolution equation (by analogy)

$$\partial_t \kappa^{II} = -\text{curl}(\kappa^{II} \times \mathbf{V})$$

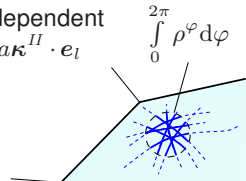
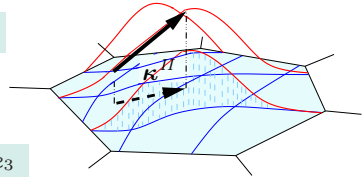
Planar projection of κ^{II}

Derivation of orientation dependent density $\rho^\varphi(x_1, x_2, \varphi, t) = a \kappa^{II} \cdot \mathbf{e}_l$

$$\int_0^{2\pi} \rho^\varphi d\varphi$$

Total dislocation density

$$\rho(x_1, x_2, t) = \int_0^{2\pi} \rho^\varphi d\varphi$$



Continuum Dislocation Dynamics (CDD)

Evolution equation of lifted dislocation density vector

$$\partial_t \kappa^{\perp} = -\text{curl}(\kappa^{\perp} \times \mathbf{V})$$

$$\kappa^{\perp} = \frac{\rho^{\varphi}}{a} \mathbf{e}_l + \rho^{\varphi} k \mathbf{e}_3$$

Averaged/Simplified Theory (sCDD)

Averaged field variables

$$\rho(x_1, x_2, t) = \int_0^{2\pi} \rho^{\varphi} d\varphi$$

$$\overline{\rho k}(x_1, x_2, t) = \int_0^{2\pi} \rho^{\varphi} k d\varphi$$

$$\kappa^{\perp} = \int_0^{2\pi} \rho^{\varphi} \mathbf{e}_{\nu} d\varphi$$

Averaged evolution equations

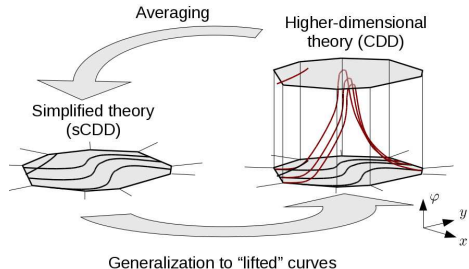
$$\partial_t \rho = -\text{div}(\kappa^{\perp} \nu) + \overline{\rho k} \nu$$

$$\partial_t \overline{\rho k} = -\text{div}\left(\frac{\overline{\rho k}}{\rho} \nu \kappa^{\perp} + \rho/2 \nabla_p \nu\right)$$

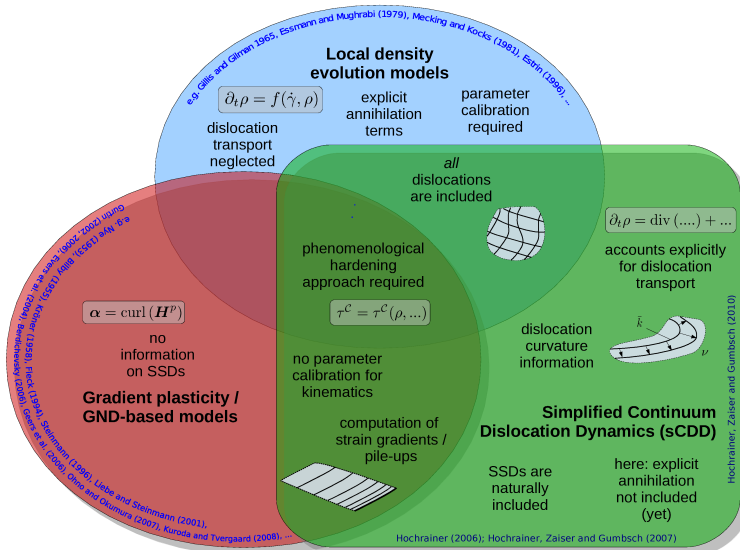
Equivalent: Evolution equations of density ρ^{φ} and curvature k

$$\partial_t \rho^{\varphi} = -\text{div}(\rho^{\varphi} \nu) - \partial_{\varphi}(\rho^{\varphi} \vartheta) + \rho^{\varphi} k \nu$$

$$\partial_t(\rho^{\varphi} k) = -\text{div}(\rho^{\varphi} k \nu - \rho^{\varphi} \vartheta \mathbf{e}_l)$$



Comparison of Dislocation Theories



Single slip framework

Additive decomposition

Plastic distortion

Elastic strain

Stress

Resolved shear stress

$$\text{grad}(\mathbf{u}) = \mathbf{H} = \mathbf{H}^e + \mathbf{H}^p$$

$$\mathbf{H}^p = \gamma \mathbf{d} \otimes \mathbf{n} = \gamma \mathbf{M}$$

$$\boldsymbol{\varepsilon}^e = \text{sym}(\mathbf{H}^e)$$

$$\boldsymbol{\sigma} = \mathbb{C}[\boldsymbol{\varepsilon}^e]$$

$$\tau = \boldsymbol{\sigma} \cdot \mathbf{M}$$

Coupling equations

Orowan equation

Overstress modell

Taylor hardening

$$\dot{\gamma} = \rho b \nu$$

$$\nu = \nu_0 \text{sgn}(\tau) \left\langle \frac{|\tau + \text{div}(\boldsymbol{\xi})| - \tau^c}{\tau^d} \right\rangle^p$$

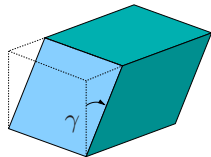
$$\tau^c = \tau_0^c + a G b \sqrt{\rho}$$

PDEs

$$\text{div}(\boldsymbol{\sigma}) = \mathbf{0}$$

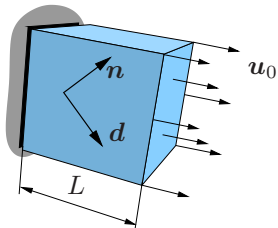
$$\partial_t \rho = -\text{div}(\boldsymbol{\kappa}^\perp \nu) + \overline{\rho k} \nu$$

$$\partial_t \overline{\rho k} = -\text{div}(\overline{\rho k} / \rho \nu \boldsymbol{\kappa}^\perp + \rho / 2 \nabla_p \nu)$$



Dislocation Starvation Simulation 1

Initial conditions

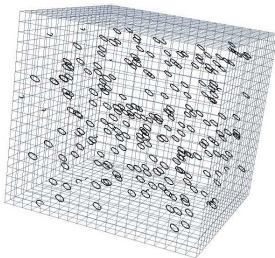


$$\begin{aligned}\rho(\mathbf{x}, t = 0) &= \rho_0 = \text{const.} \\ k(\mathbf{x}, t = 0) &= k_0 \gg 1/L \\ \Rightarrow \overline{\rho k}(\mathbf{x}, t = 0) &= \rho_0 k_0\end{aligned}$$

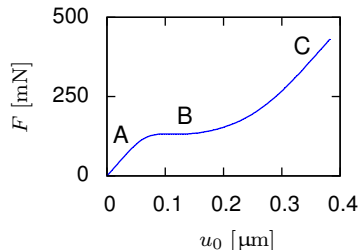
High viscosity required for stabilization

Videos 1, 2, 3

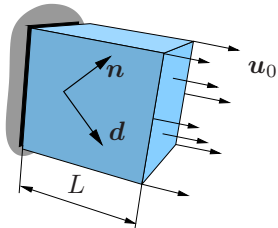
$\Rightarrow$ Homogeneous distribution of small loops



Force displacement curve



Dislocation Starvation Simulation 2



Initial conditions

$\rho(\mathbf{x}, t = 0)$: concentrated at center

$k(\mathbf{x}, t = 0) = k_0 \gg 1/L$

Videos 4, 5

⇒ Inhomogeneous distribution of small loops

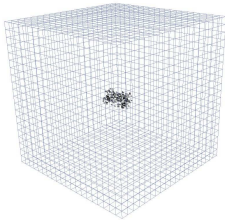


Figure: Initial configuration

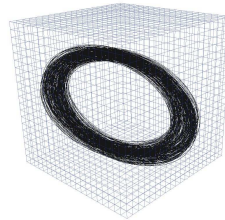
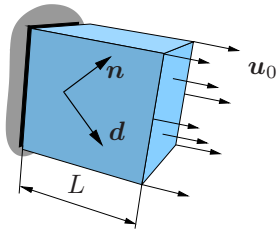


Figure: After loading



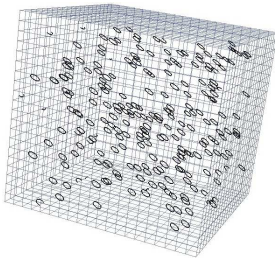
Initial conditions

$$\rho(\mathbf{x}, t = 0) = \rho_0 = \text{const.}$$

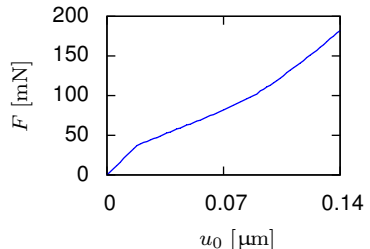
$$k(\mathbf{x}, t = 0) = k_0 \gg 1/L$$

$$\Rightarrow \overline{\rho k}(\mathbf{x}, t = 0) = \rho_0 k_0$$

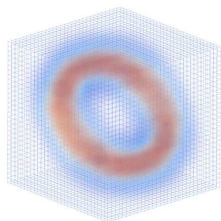
$\Rightarrow$ Homogeneous distribution of small loops



Force displacement curve



- There is a need for a continuum theory of dislocations to bridge the scales
- Concept of lifted curves $\rightarrow$ physically based continuum theory
- Takes into account
 - SSDs & GNDs
 - transport
 - curvature
- Fits into crystal plasticity framework
- Facilitates the simulation of effects like dislocation starvation



Thank you for your attention

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